



“Semi-experimental” structures demystified

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$$I_{tot} = I_{mol} + I_{at} + I_{bgl}$$

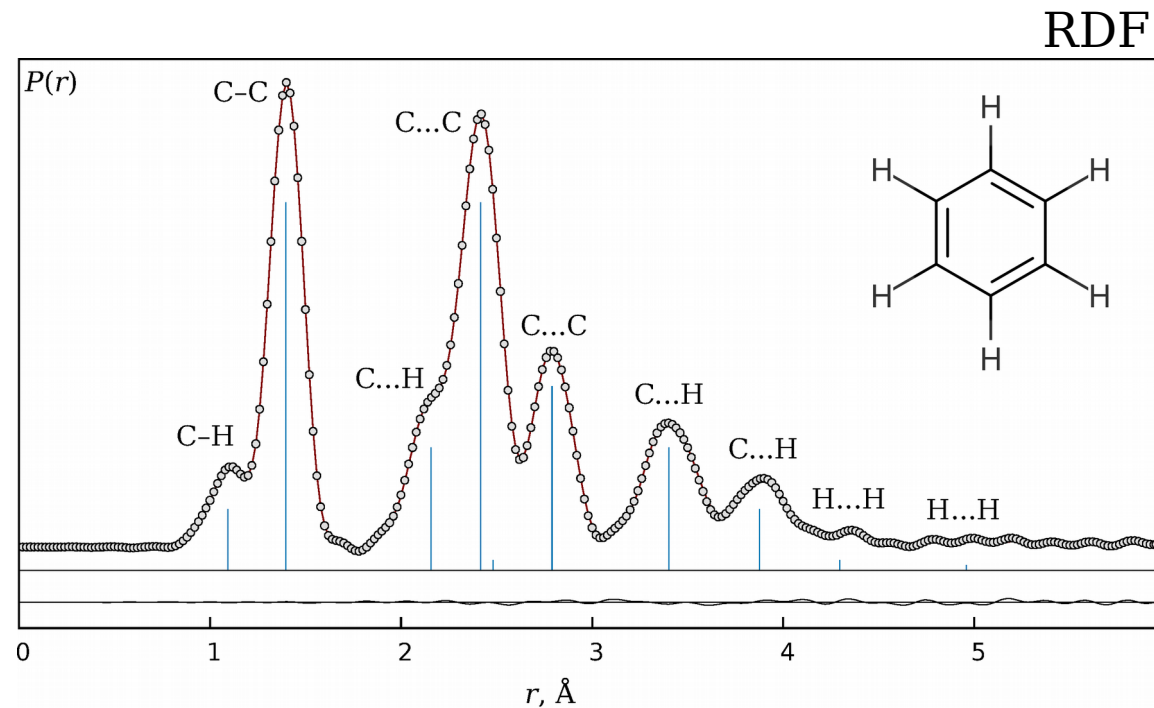
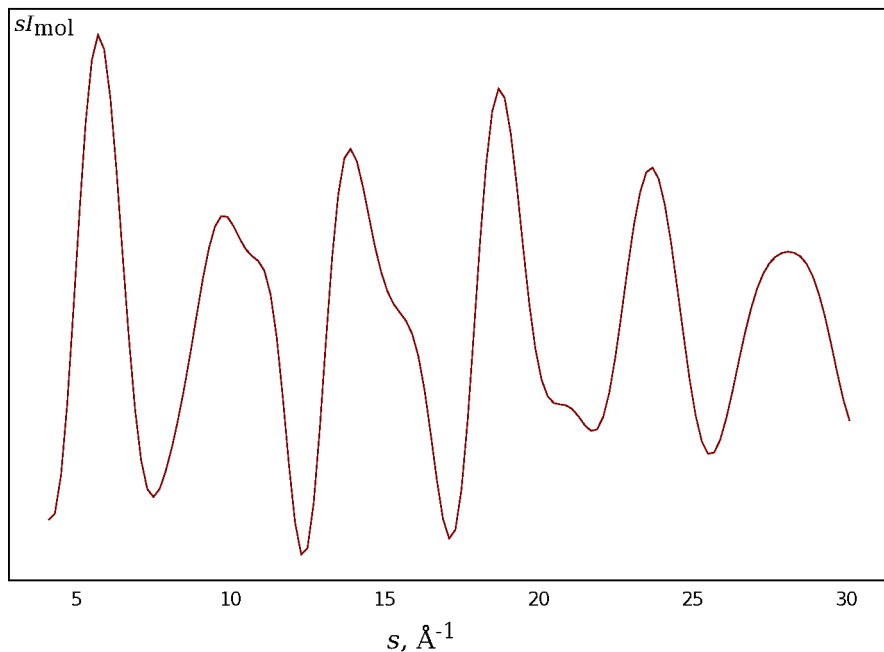
$$s = \frac{4\pi}{\lambda} \sin\left(\frac{\theta}{2}\right)$$

$$sM(s) = \frac{sI_{mol}}{I_{at}} = \sum_{i>j}^N g_{i,j} e^{-\frac{(sl_{i,j})^2}{2}} \frac{\sin(sr_{i,j} - a_{i,j}s^3)}{r_{i,j}}$$

θ - scattering angle,
 λ - electron wavelength,
 g - scattering factors,
 r - interatomic distances,
 l - amplitudes,
 a - asymmetry constants.

Inverse problem:

$$Q = \sum_i^N [sM(s|r, l, a)^{exp} - sM(s)^{model}]^2 \rightarrow min$$

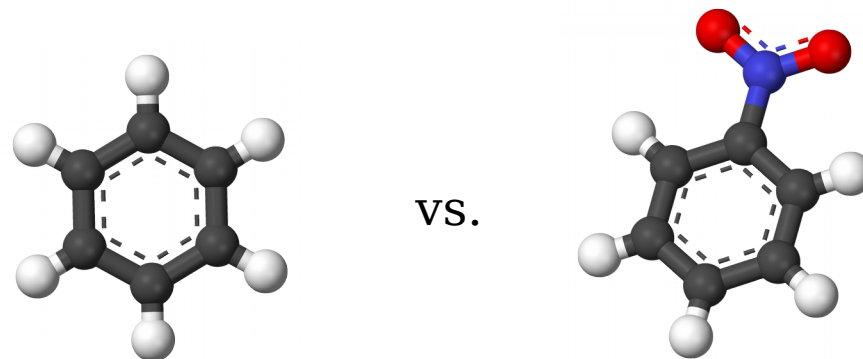


In most cases refined structures are in fact semi-experimental because of using supplementary theoretical data:

- Corrections to geometrically consistent structure (r_{h0} , r_{h1} , r_e).
- Assumed vibrational amplitudes and/or their differences.
- Assumed geometrical parameters and/or their differences.

and/or

- Regularization parameters.



How much experimental?

To which extent
is refined structure experimental
if we use supplementary theoretical data?



Lev V. Ilkov (Moscow SU)

Tikhonov's regularization in GED: Bartel's "predicate observations", SARACEN

Regularization of internal coordinates:

$$Q = \sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2 + \alpha \sum_i w_i (p_i^0 - p_i^{\text{mod}})^2 \rightarrow \min$$

$\alpha = 0 \rightarrow$ Fully experimental structure (100 % experimental info. in refined prms.)

$\alpha = \infty \rightarrow$ Fully theoretical structure (0 % exp. info. in refined prms.)

$\alpha = (0, \infty) \rightarrow$ Semi-experimental structure (???) %. Used in practice!

L. S. Bartell, D. J. Romanesko, T. C. Wong, in *Molecular Structure by Diffraction Methods*, The Chemical Society, London, 1975, Vol. 3, pp 72 - 79.

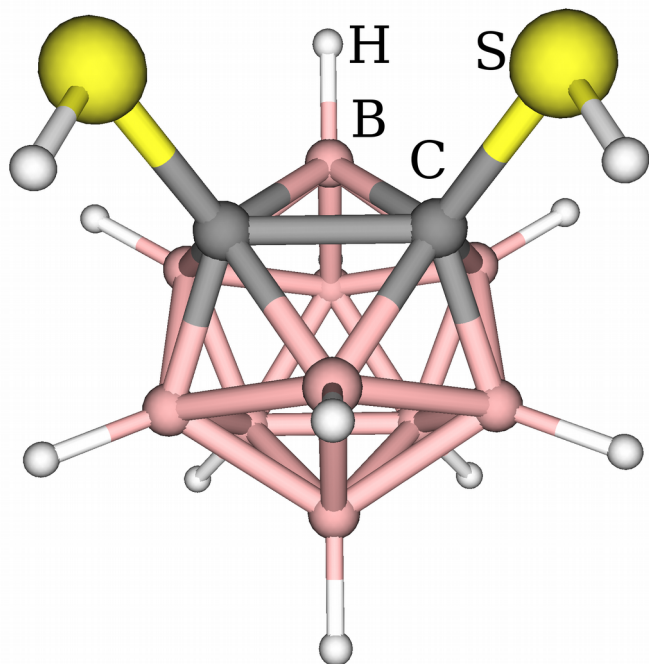
A. J. Blake, P. T. Brain, H. McNab, J. Miller, C. A. Morrison, S. Parsons, D. W. H. Rankin, H. E. Robertson, B. A. Smart, *J. Phys. Chem.*, 1996, 100, 12280.

A. N. Tikhonov, V. Y. Arsenin, *Solutions of Ill-posed Problems*, Washington, DC: V. H. Winston & Sons, 1977.

$$Q = \sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2 + \alpha \sum_i w_i (x_i^0 - x_i^{\text{mod}})^2 \rightarrow \min$$

$$R_f = 4.3 \%$$

$$\alpha = 5.0$$



	MP2/cc-pVTZ	GED	
	r_e	r_e	r_g
$r\text{C-B}$	1.704	1.702(4)	1.722(4)
$r\text{C-C}$	1.756	1.755(7)	1.765(7)
$r\text{B-B}$	1.782	1.777(5)	1.793(5)
$r\text{C-S}$	1.769	1.755(4)	1.770(4)
$\angle\text{B-C-B}$	63.4	63.3(2)	
$\angle\text{B-B-B}$	60.0	60.0(2)	
$\angle\text{S-C-C}$	118.0	118.0(1)	

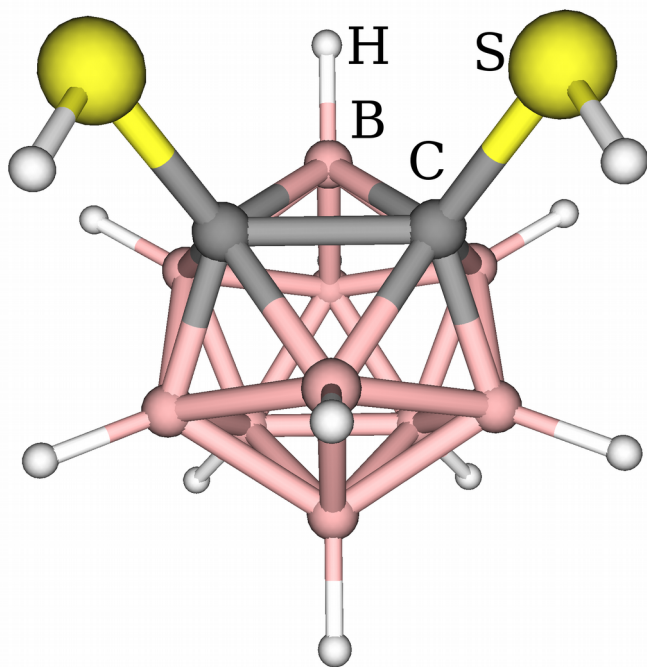
(Semi?-) Experimental Structure?

$$Q = \underbrace{\sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2}_{Q_{GED}} + \alpha \underbrace{\sum w(p^0 - p^{\text{mod}})^2}_{Q_{REG}} \rightarrow \min$$

First empirical idea: use second derivatives

$$\frac{\partial^2 Q_{GED}}{\partial p^2} \quad \frac{\partial^2 Q_{REG}}{\partial p^2}$$

$$W_{GED} = \frac{\frac{\partial^2 Q_{GED}}{\partial p^2}}{\frac{\partial^2 Q_{GED}}{\partial p^2} + \frac{\partial^2 Q_{REG}}{\partial p^2}}$$

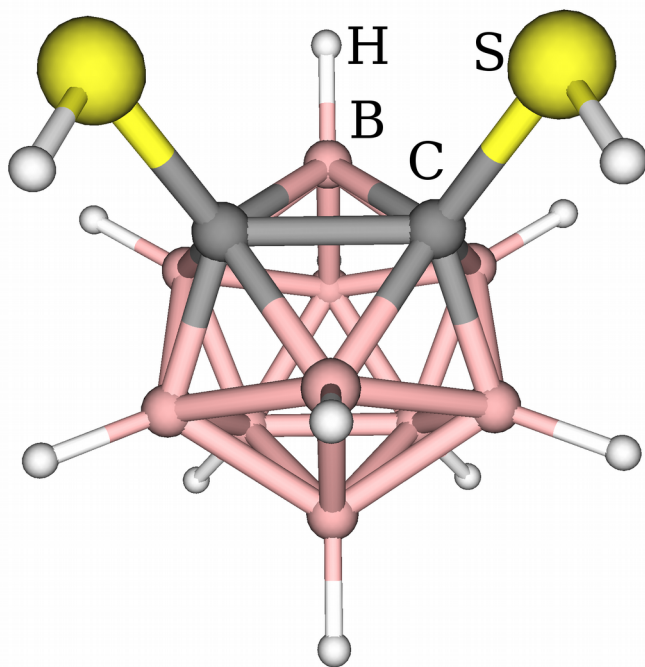


	MP2/cc-pVTZ	GED	
	r_e	r_e	w_{GED}
r_{B-H}	1.181	1.186(5)	0.001
r_{S-H}	1.339	1.341(5)	0.007
r_{C-B}	1.704	1.702(4)	0.168
r_{C-C}	1.756	1.755(7)	0.079
r_{B-B}	1.782	1.777(5)	0.176
r_{C-S}	1.769	1.755(4)	0.357
$\angle C-B-C$	61.5	61.6(2)	?
$\angle C-B-B$	58.3	58.4(2)	?
$\angle B-C-B$	63.4	63.3(2)	?
$\angle B-B-B$	60.0	60.0(2)	?
$\angle S-C-C$	118.0	118.0(1)	?
$\angle C-B-H$	116.7	116.7(3)	?
$ \angle CCSH(\text{syn}) $	95.2	95.2(2)	?

Angles: coincidence?

$$Q = \sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2 + \alpha \sum_i w_i (x_i^0 - x_i^{\text{mod}})^2 \rightarrow \min$$

Uniform regularization: $w_1 = w_2 = w_3 = \dots = 1$.

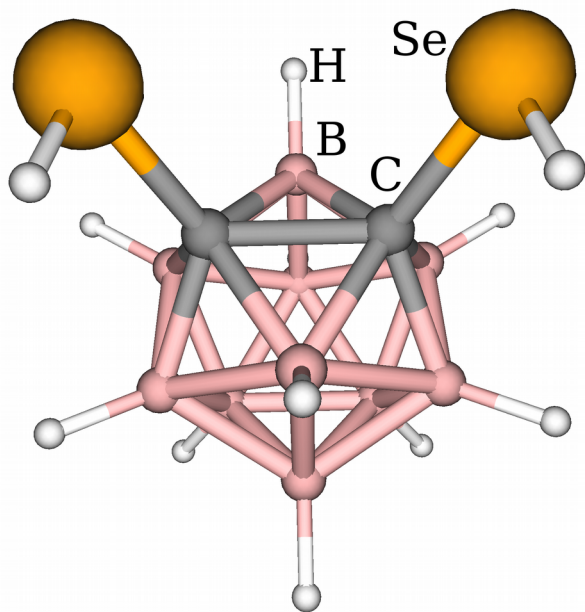


	MP2/cc-pVTZ	GED	
	r_e	r_e	w_{GED}
$\angle \text{C-B-C}$	61.5	61.6(2)	0.051
$\angle \text{C-B-B}$	58.3	58.4(2)	0.055
$\angle \text{B-C-B}$	63.4	63.3(2)	0.053
$\angle \text{B-B-B}$	60.0	60.0(2)	0.036
$\angle \text{S-C-C}$	118.0	118.0(1)	0.128
$\angle \text{C-B-H}$	116.7	116.7(3)	0.015
$ \angle \text{CCSH}(\text{syn}) $	95.2	95.2(2)	0.000₇

Low w_{GED} for Angles!

No problem, decrease α , but be ready to pay for this!

$$Q = \sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2 + \alpha \sum_i w_i (x_i^0 - x_i^{\text{mod}})^2 \rightarrow \min$$



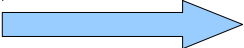
	MP2/ cc-pVTZ	GED			
		$\alpha = 0.7$		$\alpha = 43$	
	r_e	r_e	w	r_e	w
$r_{\text{C-C}}$	1.731	1.750(28)	0.933	1.726(5)	0.172
$r_{\text{B-B}}$	1.782	1.777(19)	0.943	1.775(3)	0.236
$r_{\text{C-Se}}$	1.904	1.902(10)	0.987	1.904(3)	0.521
$\angle_{\text{Se-C-C}}$	119.2	119.2(4)	0.971	119.3(1)	0.319
$\angle_{\text{Se-C-B}}$	118.9	119.1(9)	0.908	118.9(2)	0.172
$\angle_{\text{B-B-H}}$	123.1	123.0(12)	0.506	123.1(2)	0.016
$R_f, \%$	10.8	4.0		5.1	

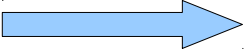
General form of functional: $\Phi = \sum_i \Phi_i \rightarrow \min$

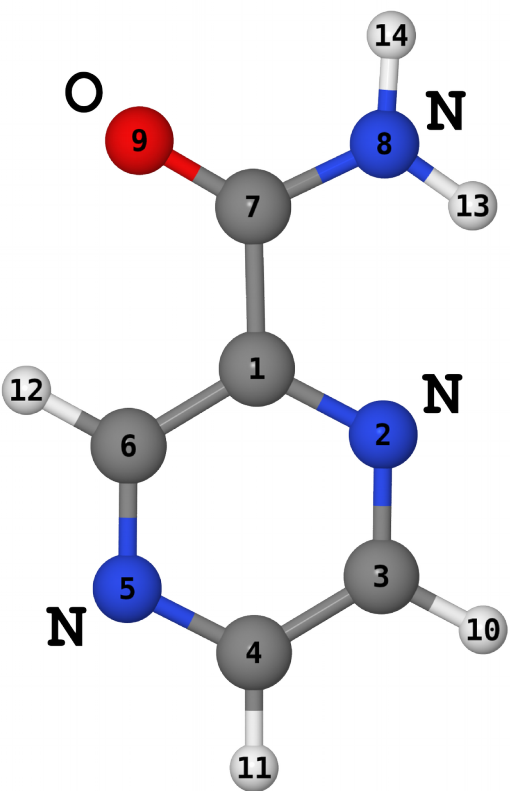
Associated distributions
(Gaussian approximation): $p_i = \frac{1}{\sqrt{2\pi}\sigma_i} \exp\left(\frac{-(\xi - \mu_i)^2}{2\sigma_i^2}\right)$

Kullback-Leibler divergence: $J(f_1, f_2) = \int f_1 \ln\left(\frac{f_2}{f_1}\right) dx + \int f_2 \ln\left(\frac{f_1}{f_2}\right) dx$

Derivatives: $a_i^{(k)} = \frac{\partial^k \Phi_i}{\partial \xi^k}$ $a^{(k)} = \sum_i a_i^{(k)}$

 $J(p_i, p) = \frac{1}{2} \left[\left(\frac{a_i^{(1)}}{a_i^{(2)}} - \frac{a^{(1)}}{a^{(2)}} \right)^2 (a_i^{(2)} + a^{(2)}) + \frac{a_i^{(2)}}{a_i^{(2)}} + \frac{a_i^{(2)}}{a^{(2)}} - 2 \right]$

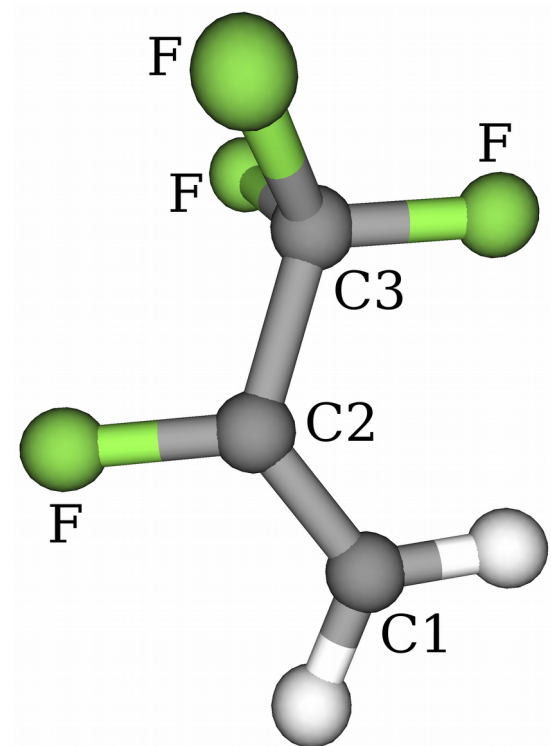
 $w_i = \frac{\frac{1}{J(p_i, p)}}{\sum_j \frac{1}{J(p_j, p)}} = \frac{1}{1 + J(p_i, p) \sum_{j \neq i} \frac{1}{J(p_j, p)}}$



	MP2(full)/ cc-pwCVTZ	GED		
	r_e	r_e	w12	w2
r_{C1-N2}	1.336	1.341(2)	1.00	0.96
r_{C1-C6}	1.391	1.404(2)	1.00	0.96
r_{C3-H10}	1.081	1.082(4)	0.02	0.21
$\angle N2-C3-C4$	122.0	122.1(2)	0.90	0.68
$\angle N8-C7-O9$	125.2	124.9(2)	1.00	0.88
$\angle (X-C3-H10)_{av}$	119.1	119.0(3)	0.26	0.39
$\angle H13-N8-H14$	121.8	121.8(3)	0.00	0.03

Consistent results

$$Q = \underbrace{\sum [sM(s)^{\text{exp}} - sM(s)^{\text{mod}}]^2}_{Q_{\text{GED}}} + \alpha \underbrace{\sum w(B^{\text{exp}} - B^{\text{mod}})^2}_{Q_{\text{ROT}}} \rightarrow \min$$



Parameter	Calcd.	MW	GED	GED+MW	w_{GED}
$r_{\text{C1-C2}}$	1.323	1.319(2)	1.324(1)	1.317(1)	0.15
$r_{\text{C2-C3}}$	1.503	1.503(2)	1.494(1)	1.497(1)	0.15
$r_{\text{C2-F}}$	1.335	1.333(1)	1.333(1)	1.334(1)	0.23
$r_{\text{(C3-F)}_{\text{av}}}$	1.333	1.333(1)	1.334(1)	1.335(1)	0.23
$r_{\text{(C1-H)}_{\text{av}}}$	1.078	1.070(29)	1.098(4)	1.085(3)	0.36
$\angle \text{C1-C2-C3}$	125.9	126.1(1)	124.7(1)	125.8(1)	0.22
$\varphi_{\text{C1-C2-C3-F}}$	120.3	120.5(1)	121.5(1)	120.5(1)	0.02
R_f %			4.45	4.72	

Calcd. = full-CCSD(T)/cc-pwCVTZ

GED+MW: $|B^{\text{exp}} - B^{\text{mod}}|$ were approx. 1% of dB .

Thank you for your attention!